

Design IV

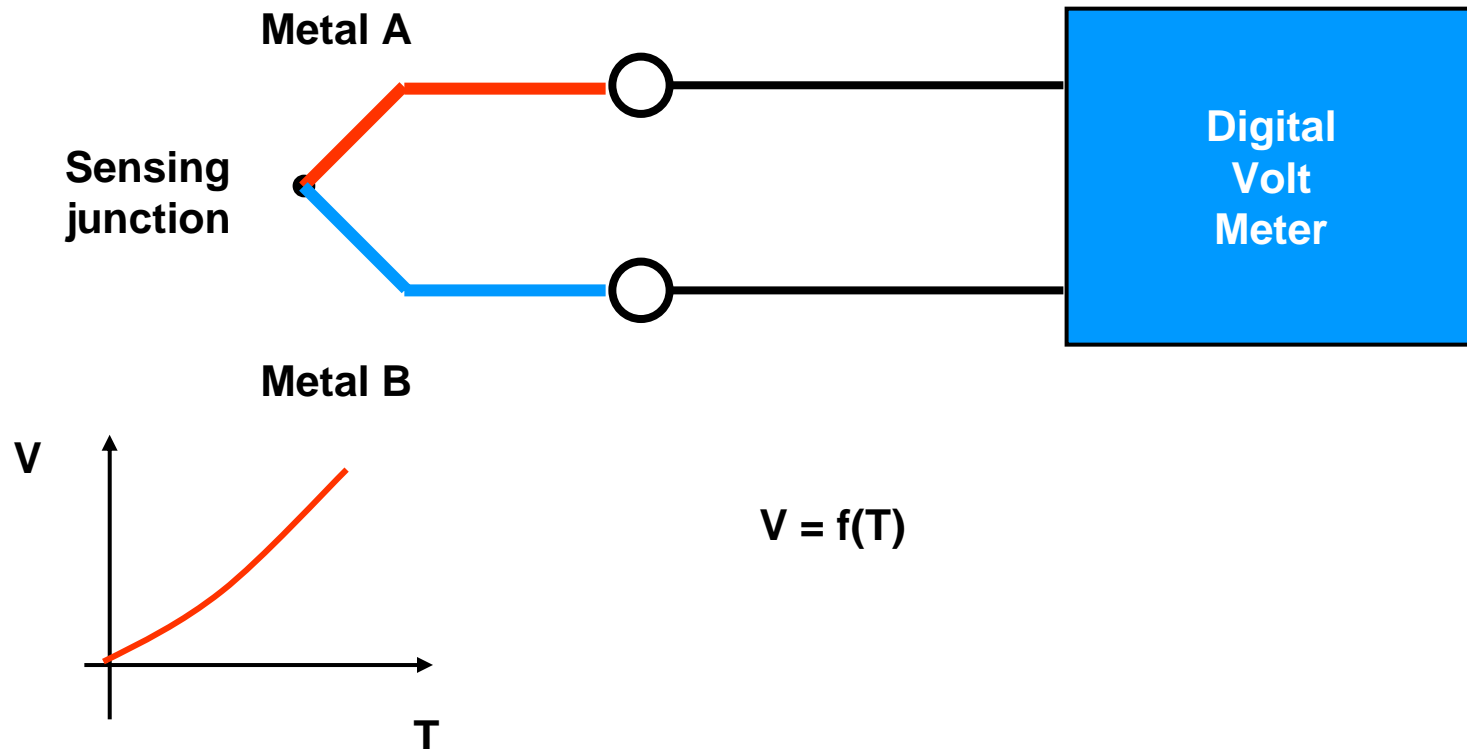
E232 Fall 07

Class 23

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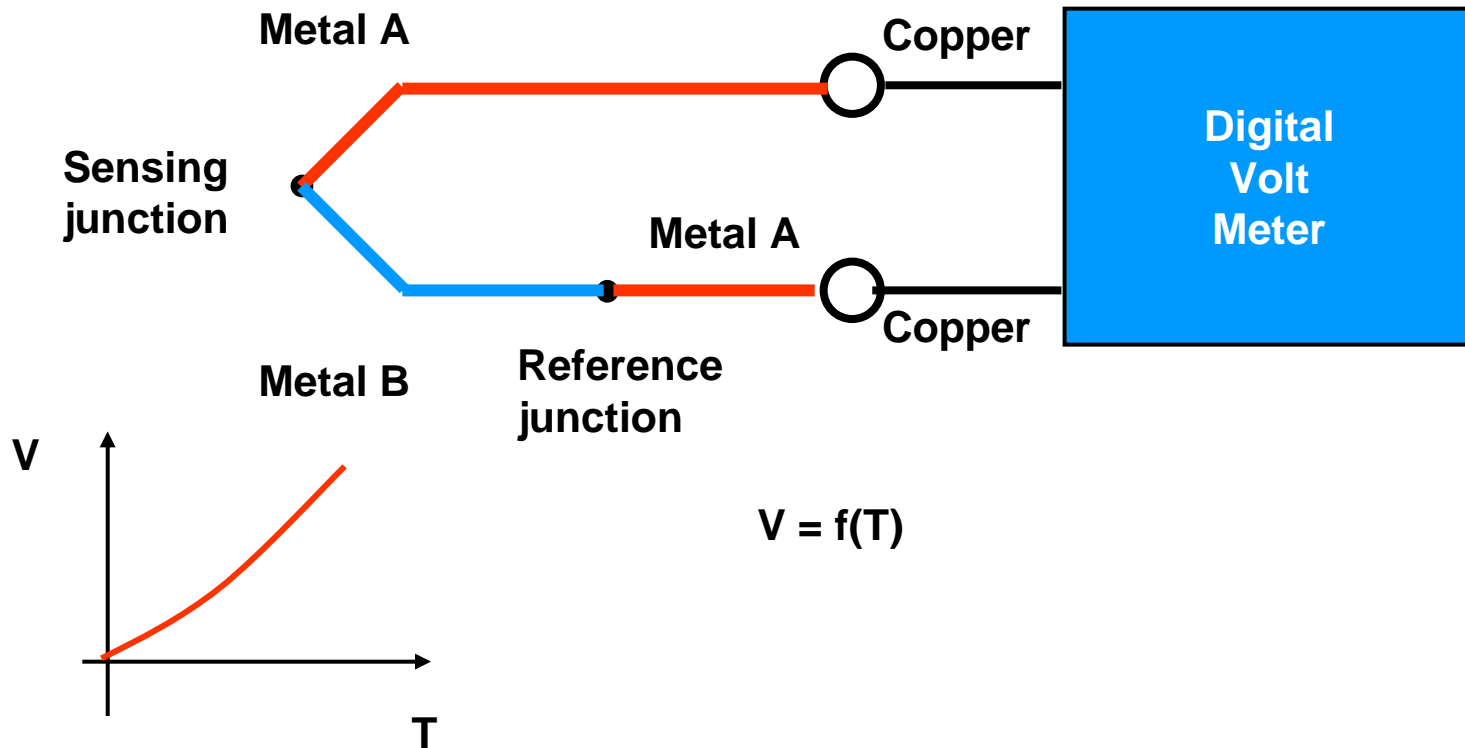
Measuring Temperature

- Thermocouples



Measuring Temperature

- Thermocouples

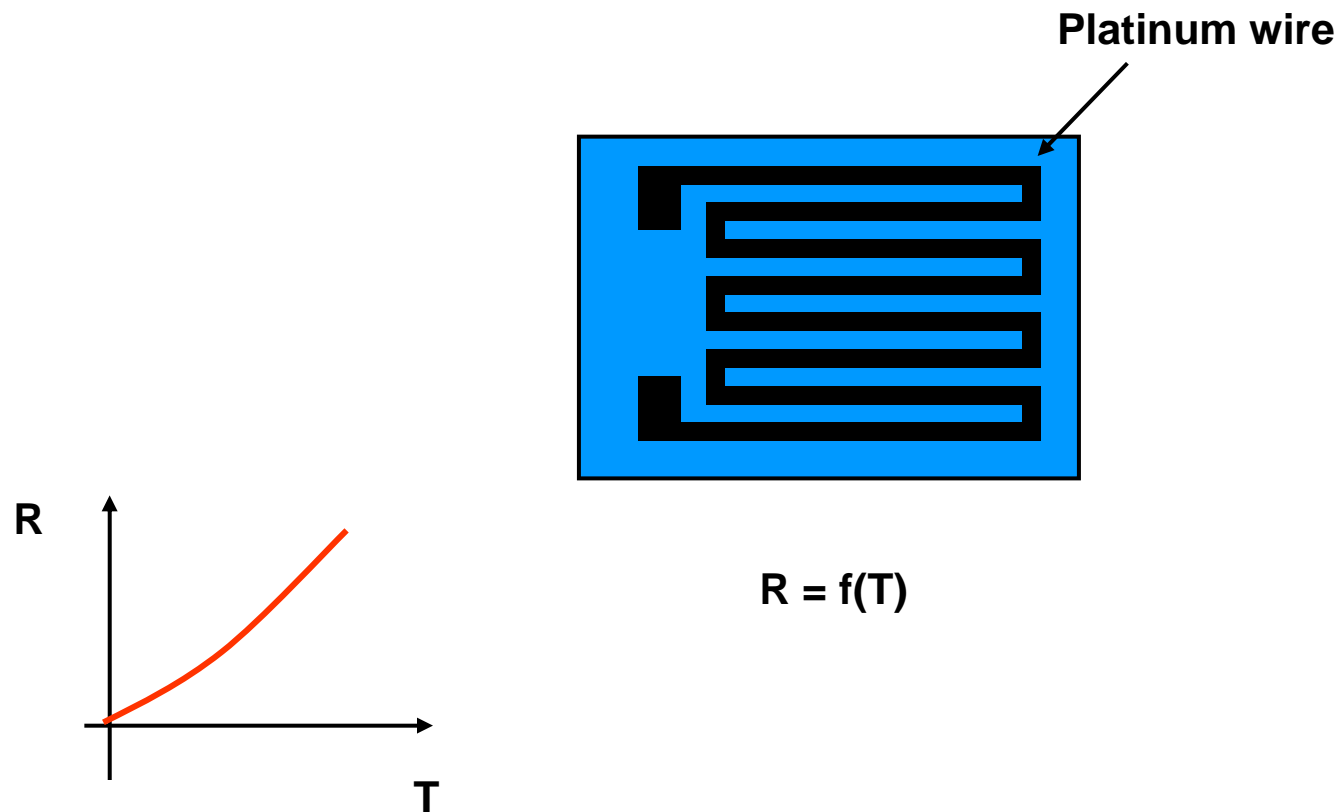


Today's topics

- Measurement sensors
 - **More temperature sensors**
 - **Non-contact temperature sensors**
 - **Fluid Flow Rate**

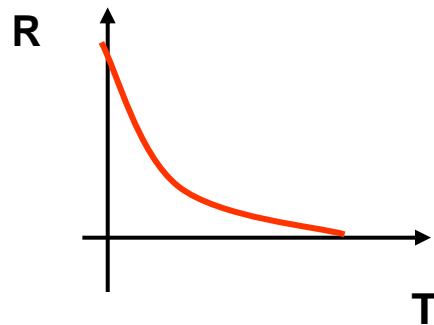
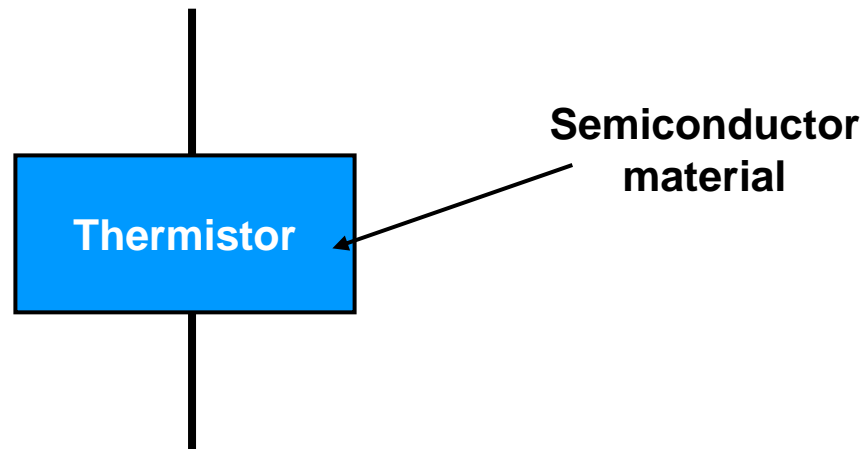
Measuring Temperature

- Resistance-Temperature Detectors



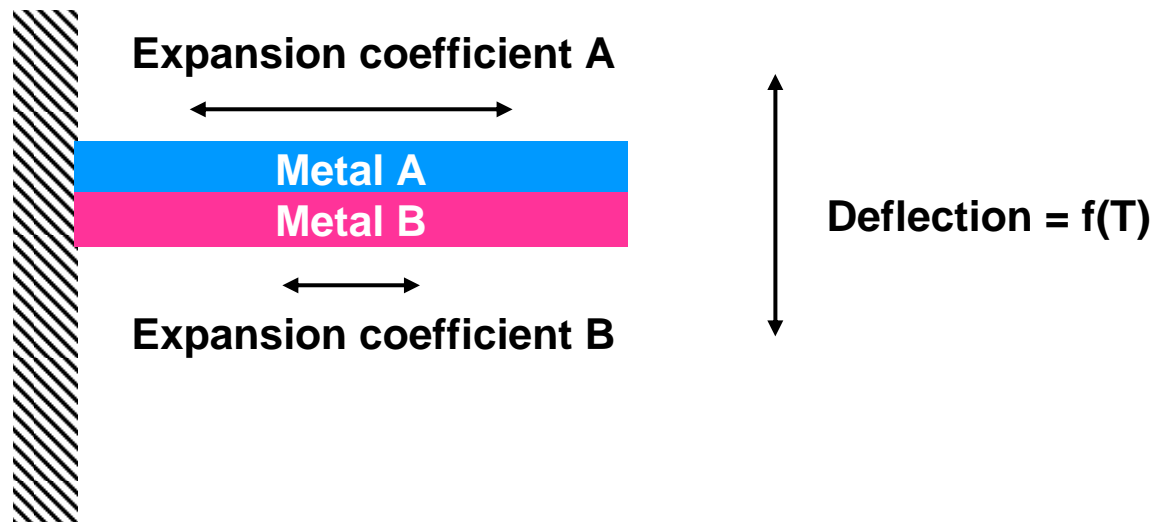
Measuring Temperature

- Thermistors



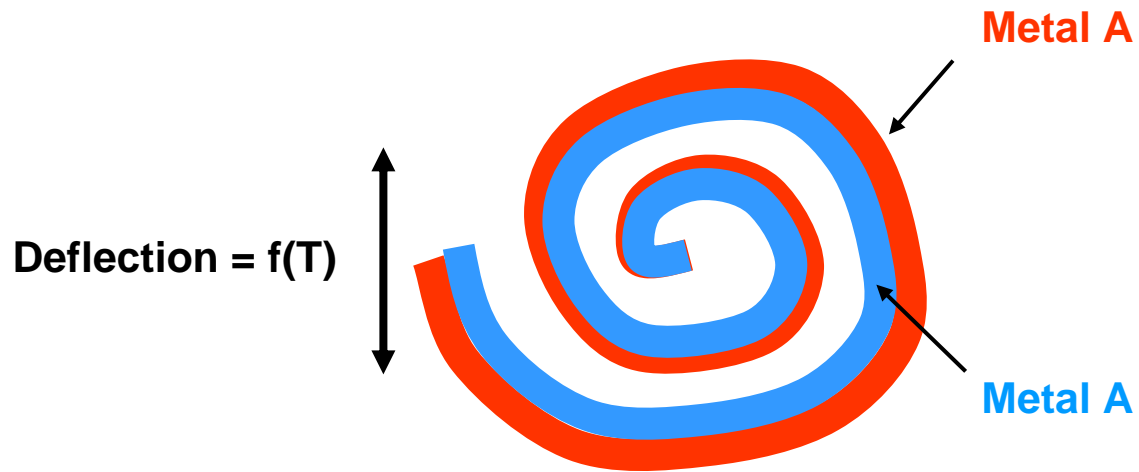
Temperature Measurement

- Linear bi-metallic strip



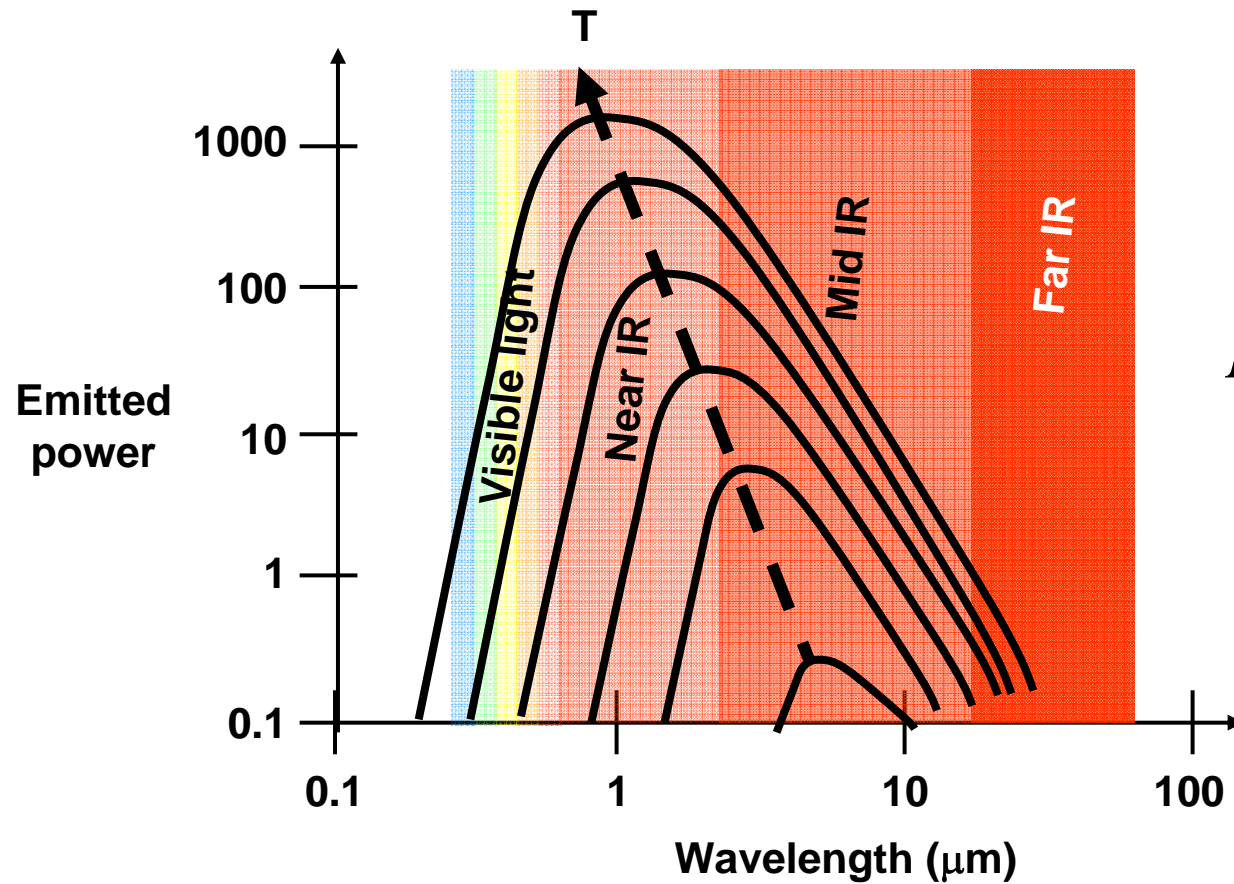
Temperature Measurement

- Spiral bi-metallic strip



Non-contact Temperature Measurement

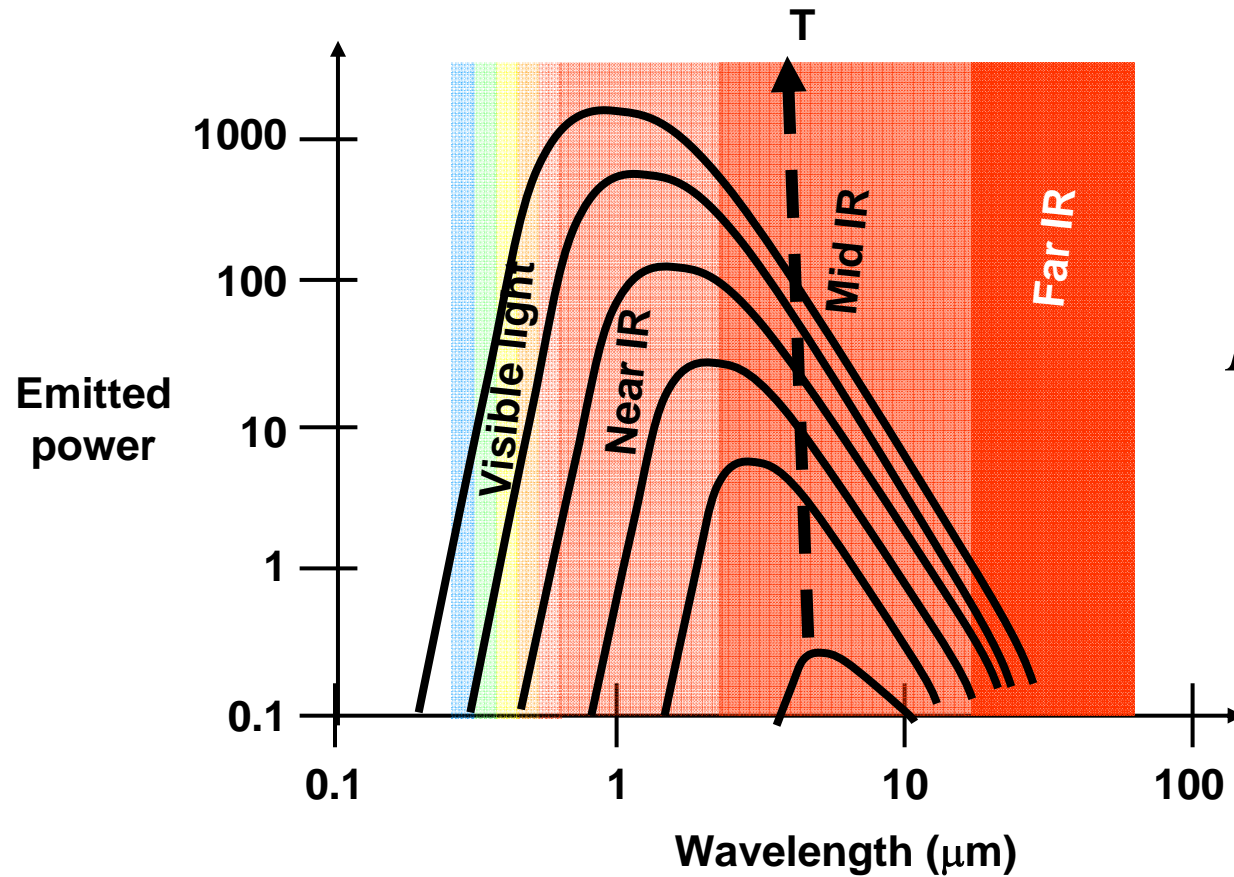
- Blackbody radiation



$$E_{b\lambda} = \frac{C_1 \lambda^{-5}}{e^{\frac{C_2}{\lambda T}} - 1}$$

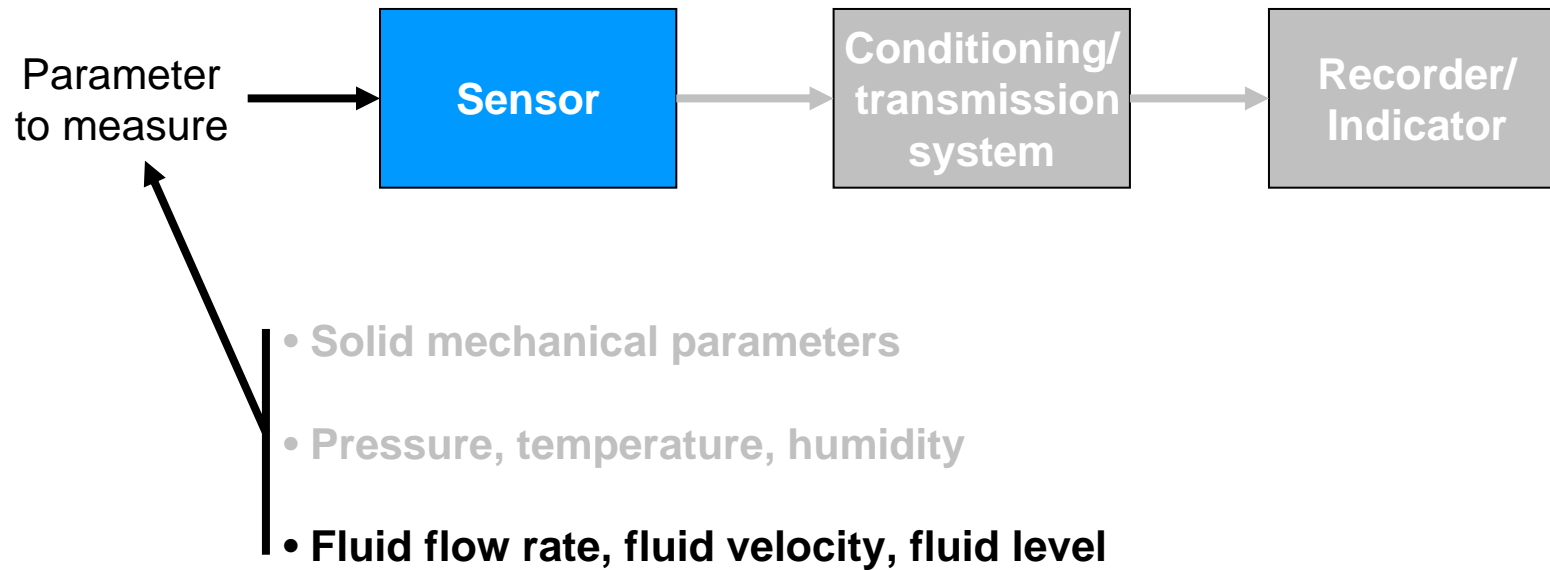
Non-contact Temperature Measurement

- Blackbody radiation



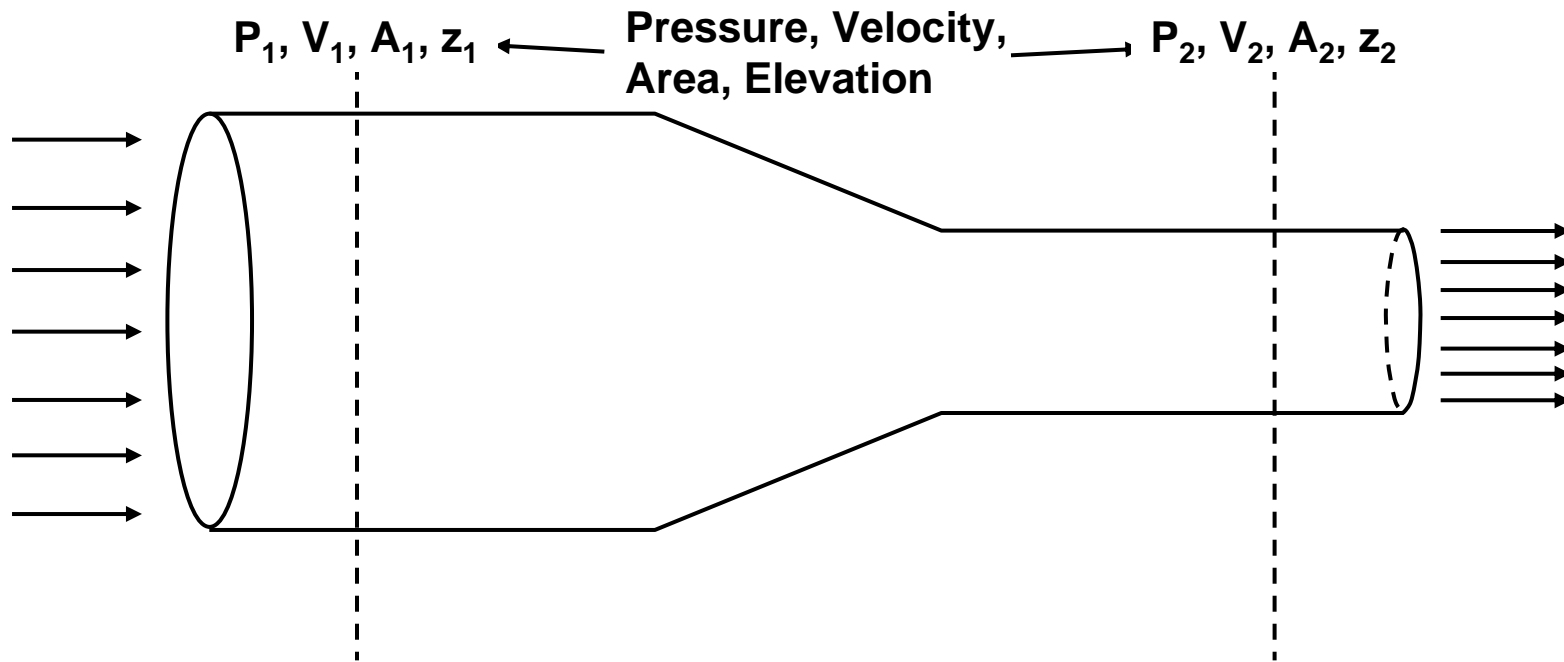
$$E_{b\lambda} = \frac{C_1 \lambda^{-5}}{e^{\frac{C_2}{\lambda T}} - 1}$$

Measurement Systems



Bernoulli Equation

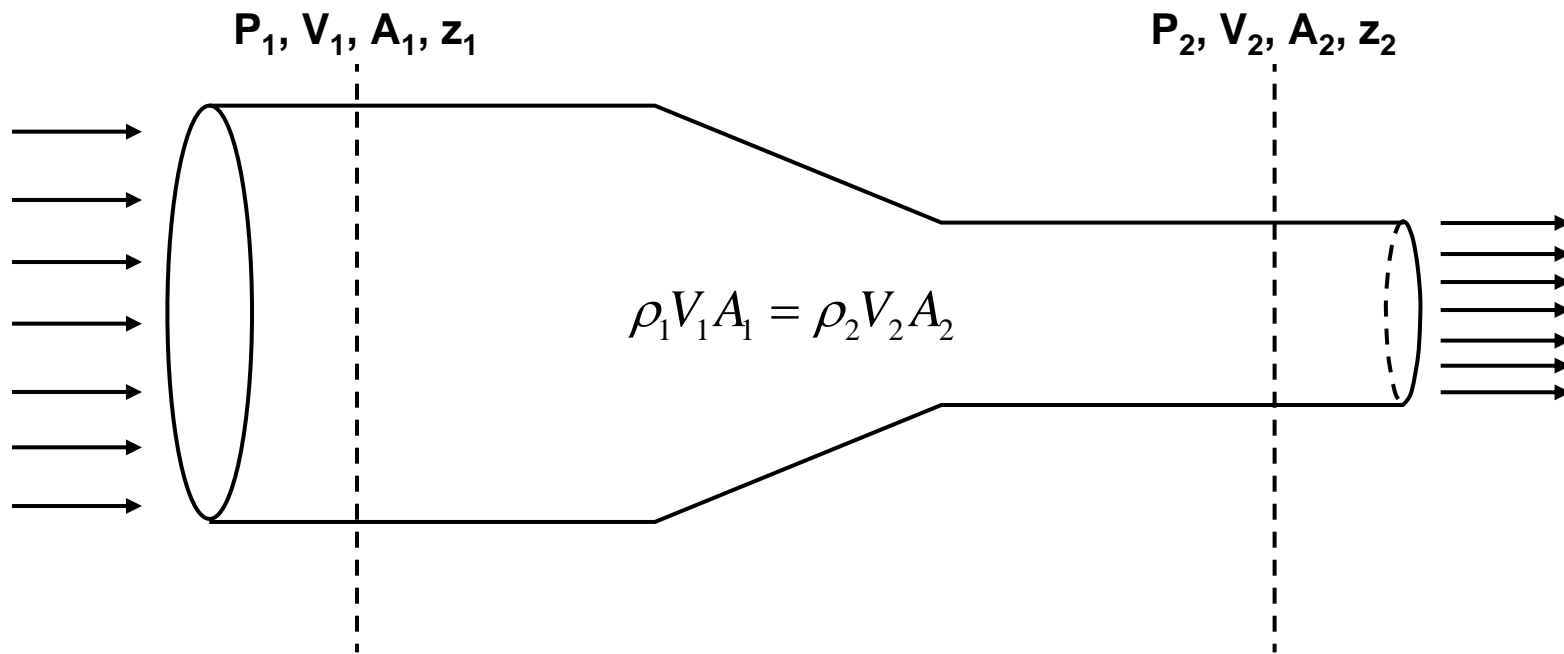
- Consider a frictionless duct with an incompressible fluid



$$\frac{V_1^2}{2} + \frac{P_1}{\rho} + gz_1 = \frac{V_2^2}{2} + \frac{P_2}{\rho} + gz_2$$

Mass flow in = mass flow out

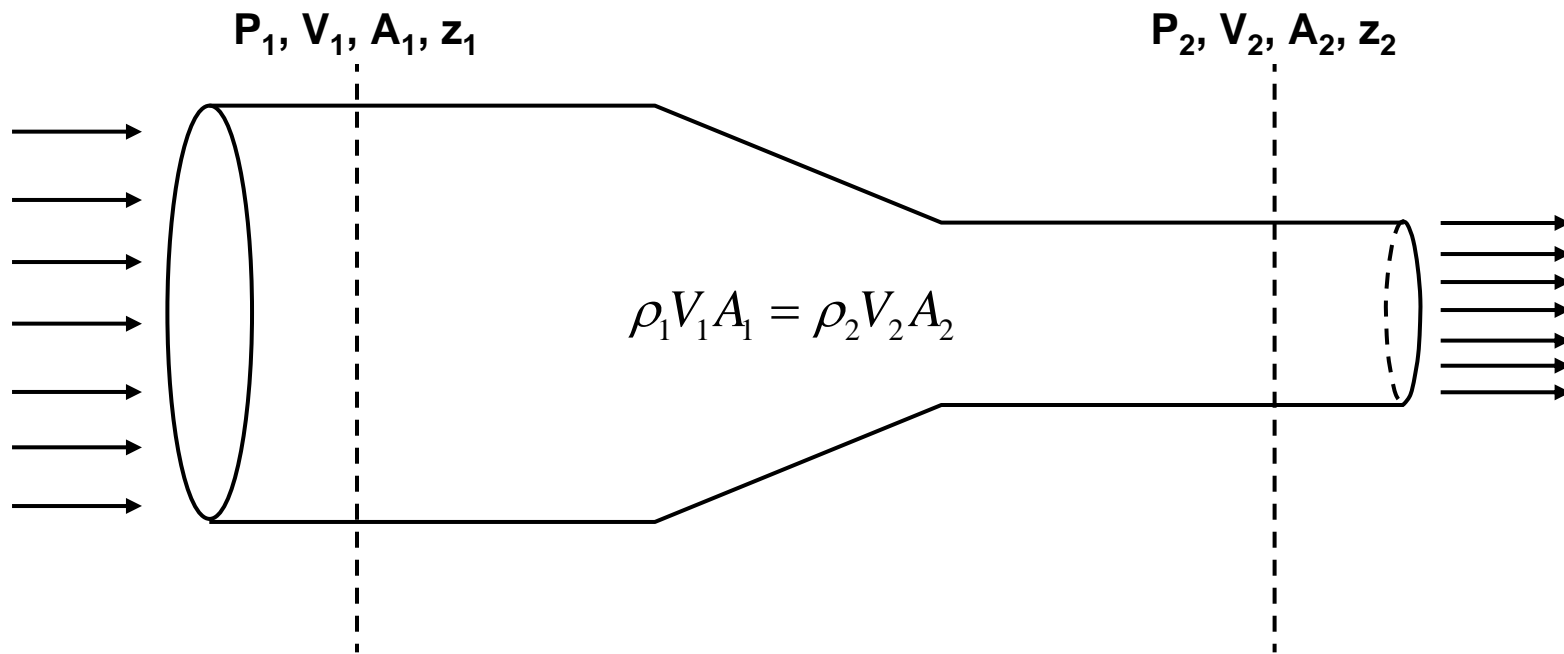
- For compressible or incompressible fluids



If $\rho_1 = \rho_2$

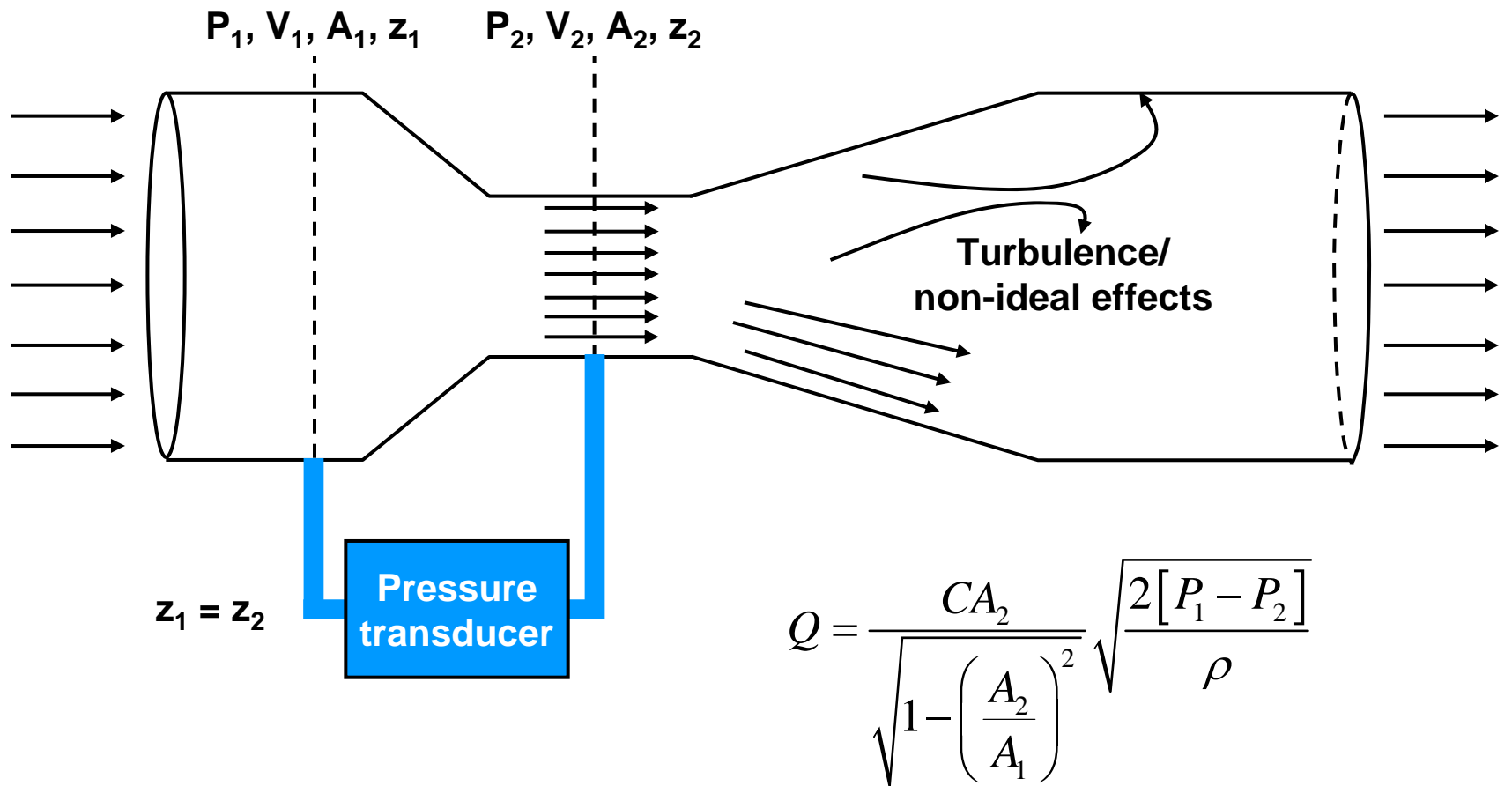
$$V_1 A_1 = V_2 A_2 = Q$$

Flow Rate

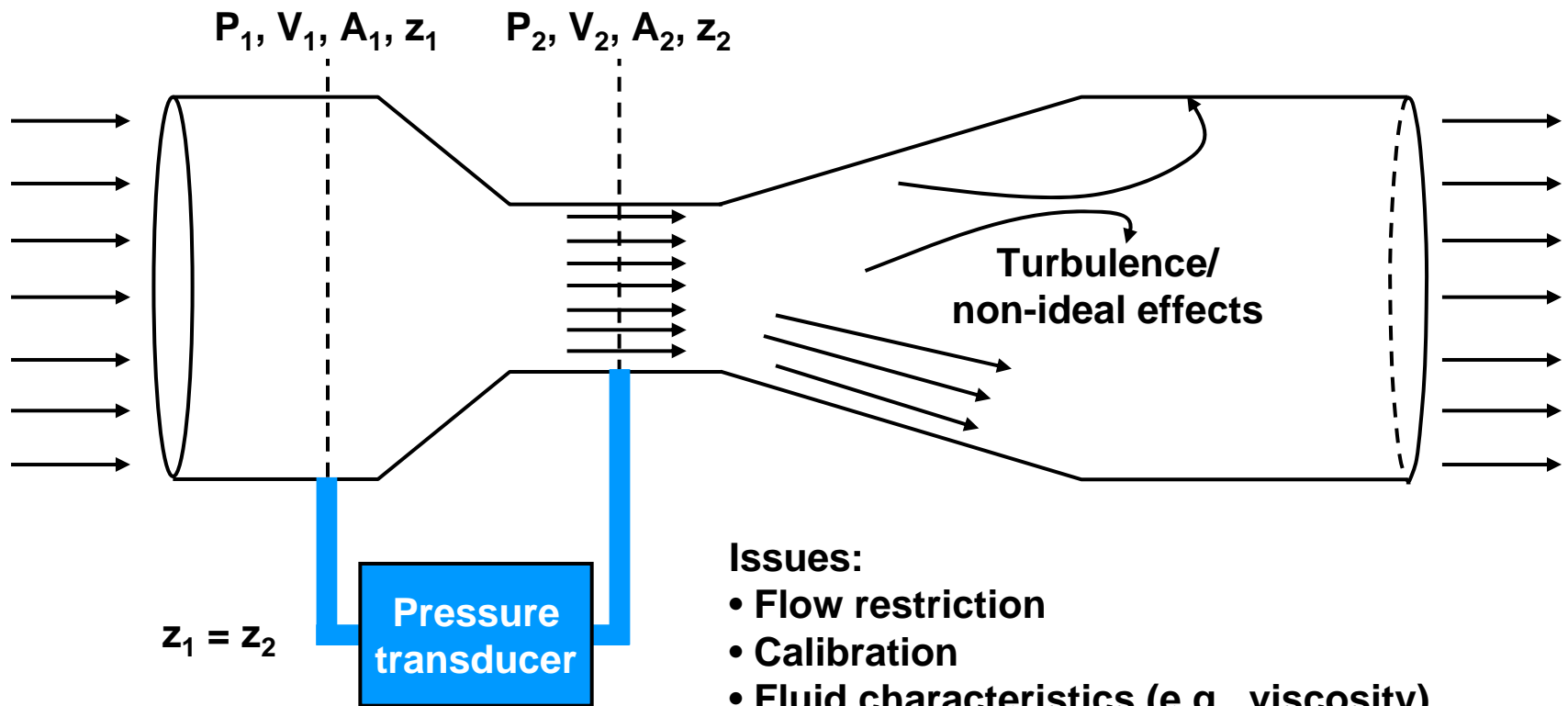


$$Q = \frac{A_2}{\sqrt{1 - \left(\frac{A_2}{A_1}\right)^2}} \sqrt{\frac{2[(P_1 + g\rho z_1) - (P_2 + g\rho z_2)]}{\rho}}$$

Venturi Tube



Venturi Tube

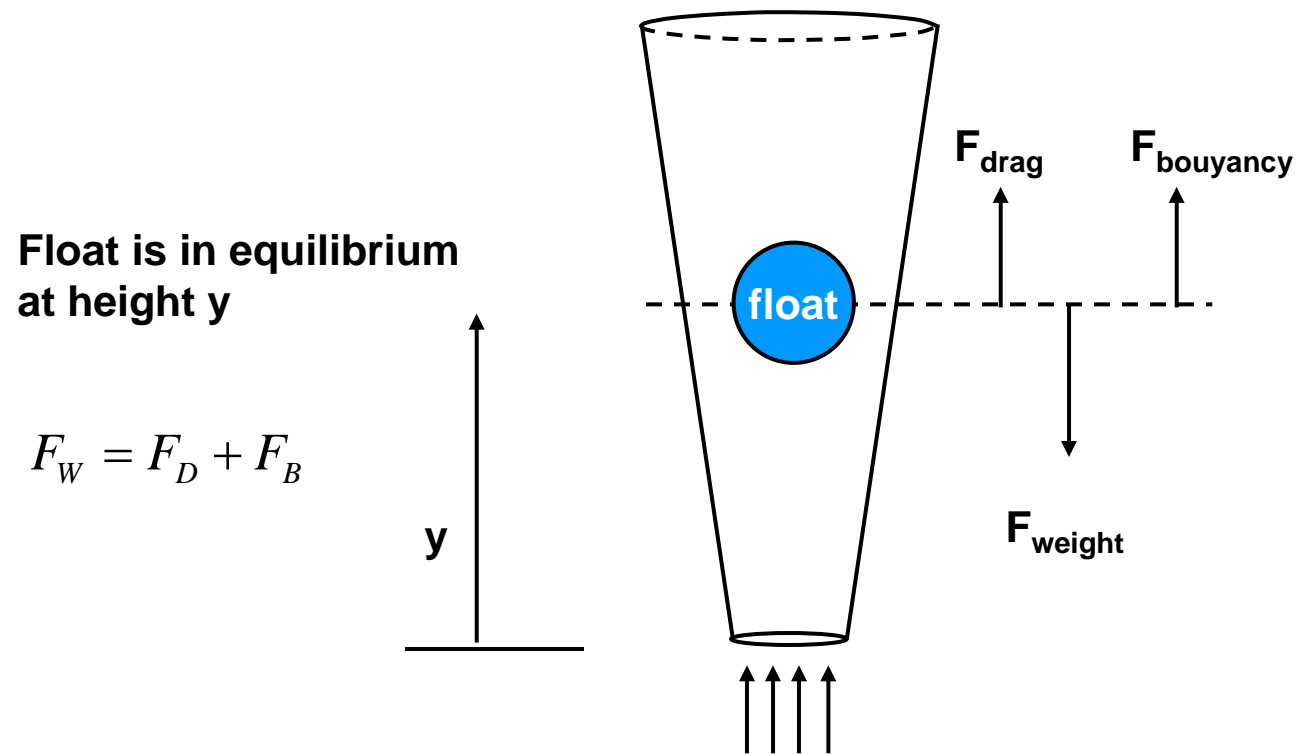


Issues:

- Flow restriction
- Calibration
- Fluid characteristics (e.g., viscosity)
- Low flow rate limitations

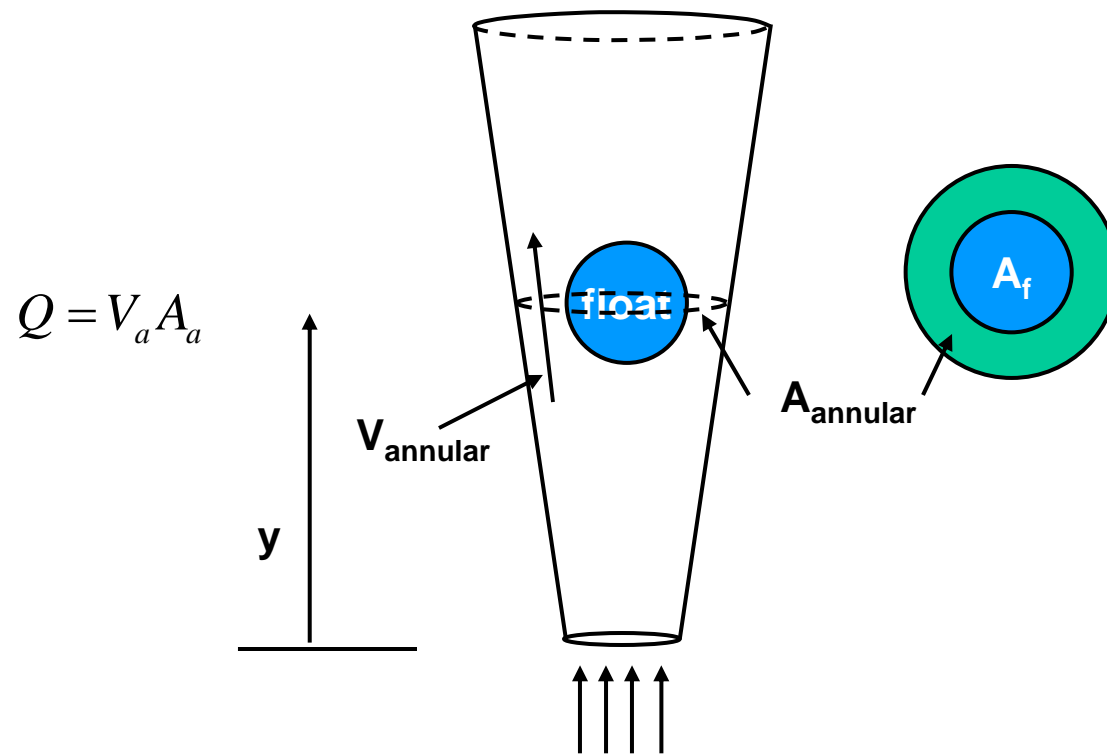
Variable-Area Flowmeters

- Rotameter



Variable-Area Flowmeters

- Rotameter



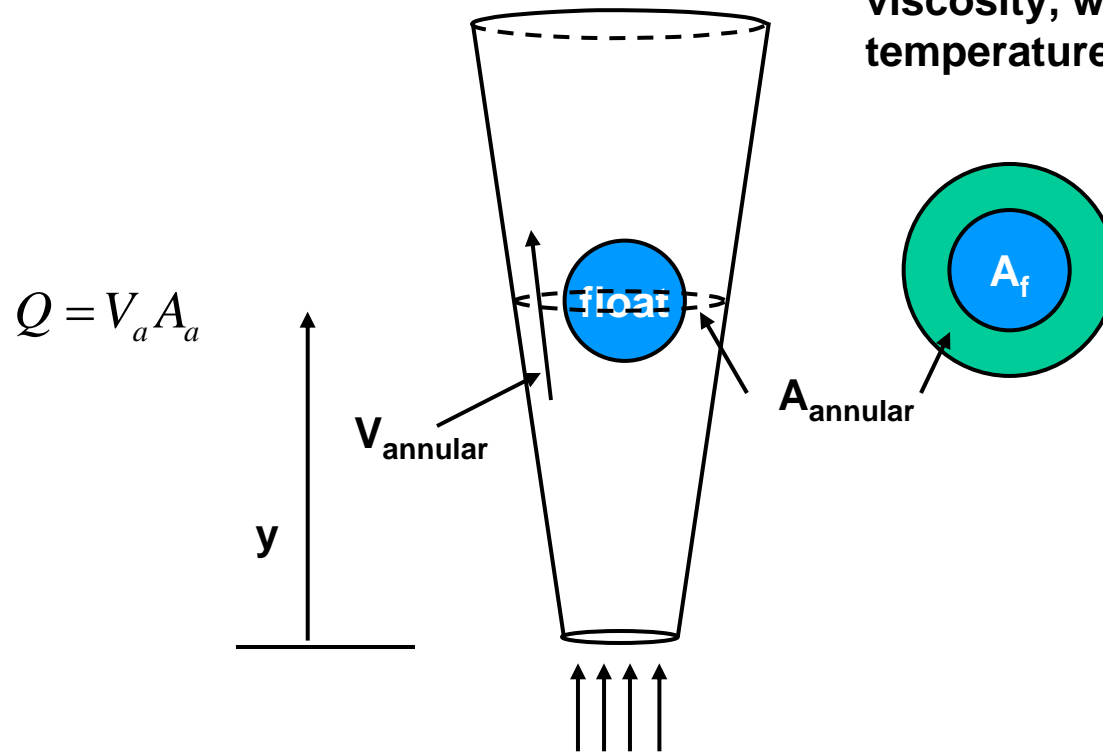
Design float so V_a is constant
Design flowmeter so A_a is linear with y

Variable-Area Flowmeters

- Rotameter

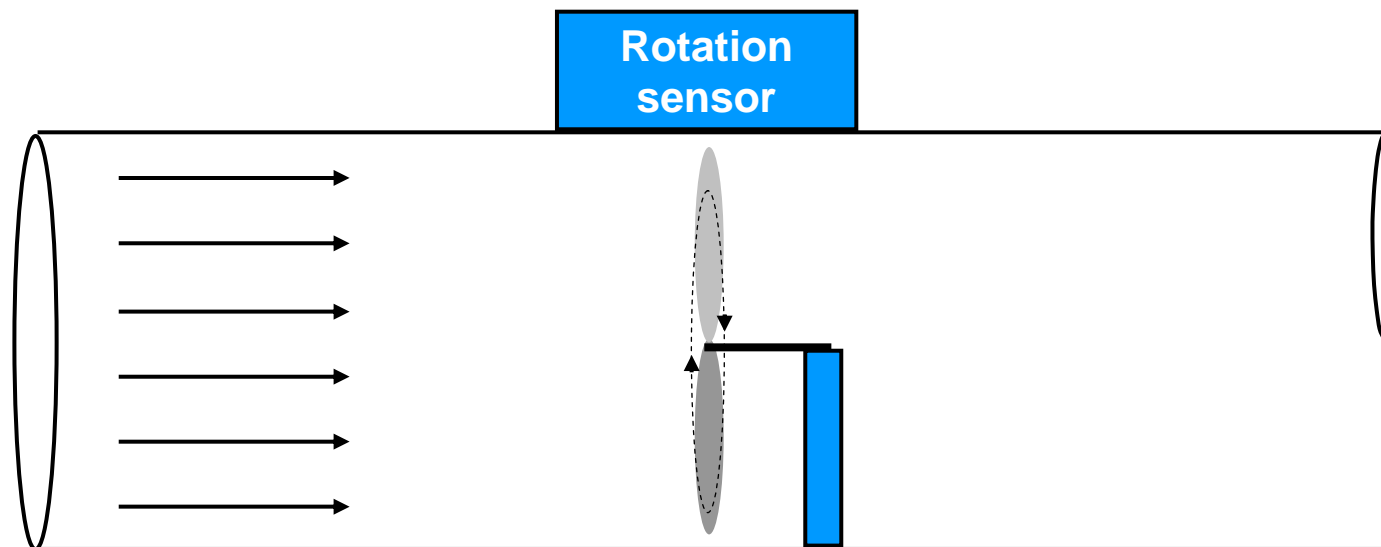
Issues:

- Rotameter design is sensitive to fluid characteristics, e.g., viscosity, which changes with temperature

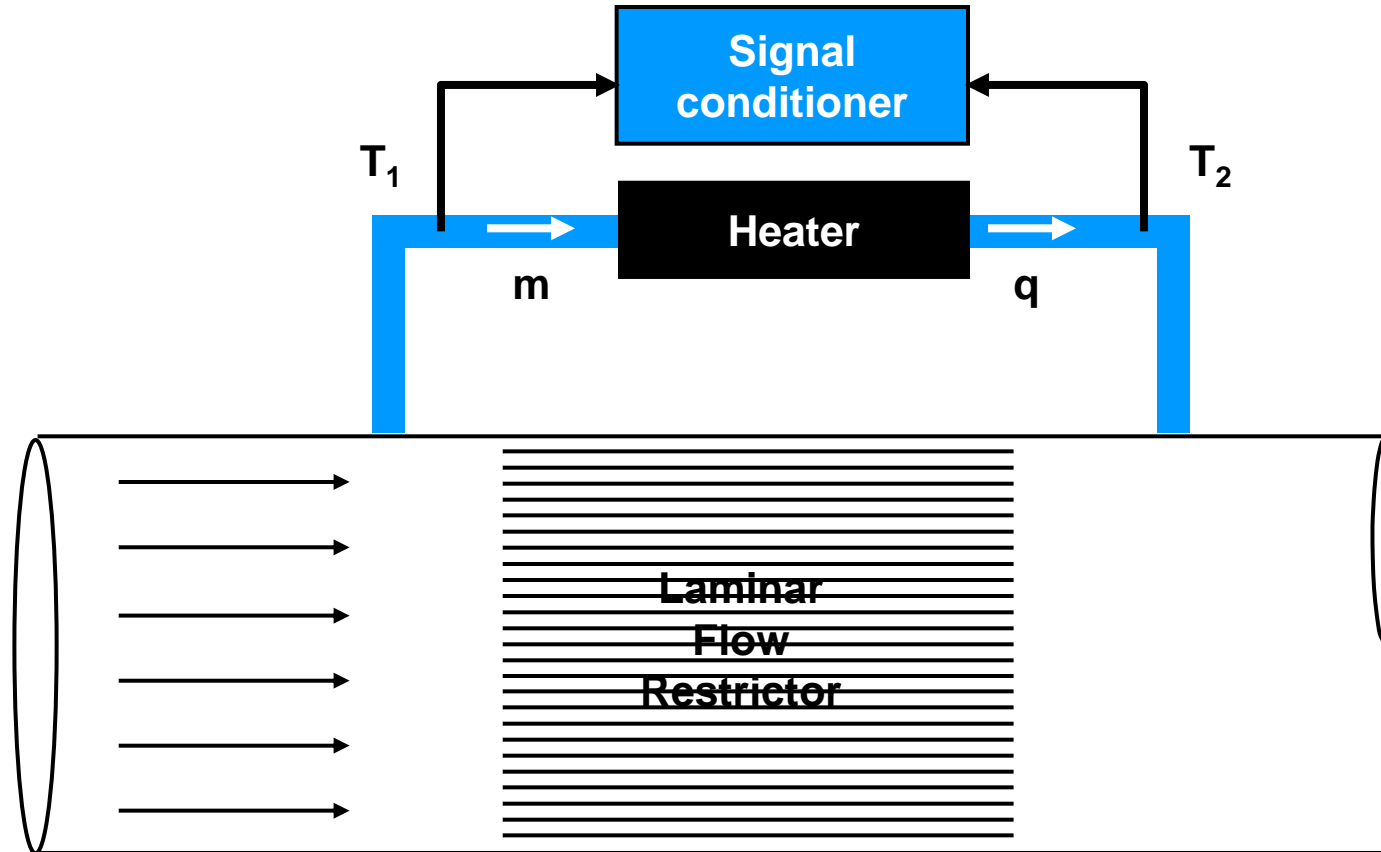


Design float so V_a is constant
Design flowmeter so A_a is linear with y

Turbine Flowmeters



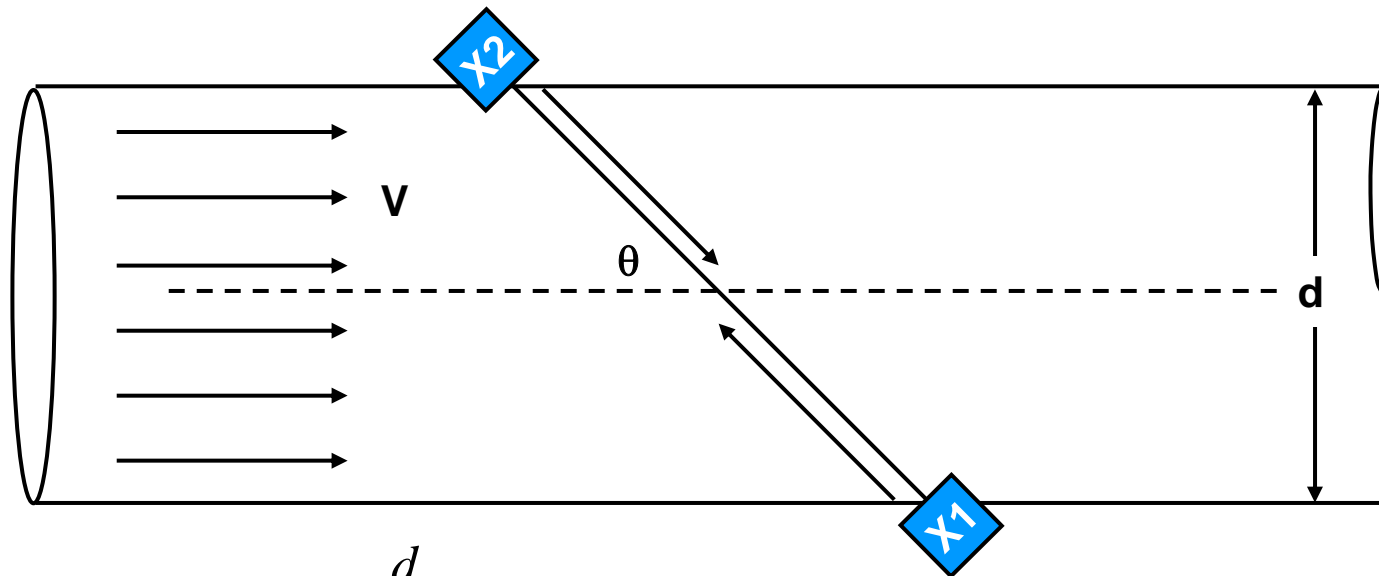
Thermal Mass Flowmeters



$$\dot{m} = \frac{q}{c_p (T_2 - T_1)}$$

Ultrasonic Transit Time Flowmeters

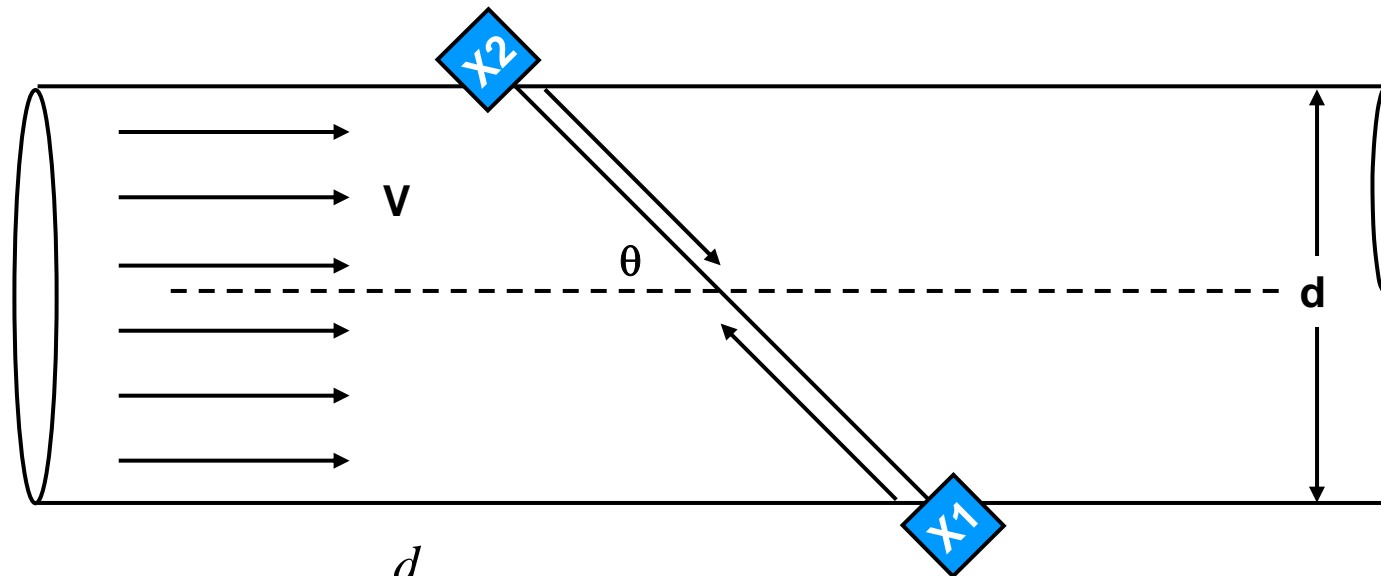
- With speed of sound in liquid, $C=f(T, P, \rho)$



$$T_{1,2} = \frac{d}{\sin(\theta)(C + V \cos(\theta))}$$

Ultrasonic Transit Time Flowmeters

- Measuring transit time in both directions makes measurement independent of speed of sound in liquid

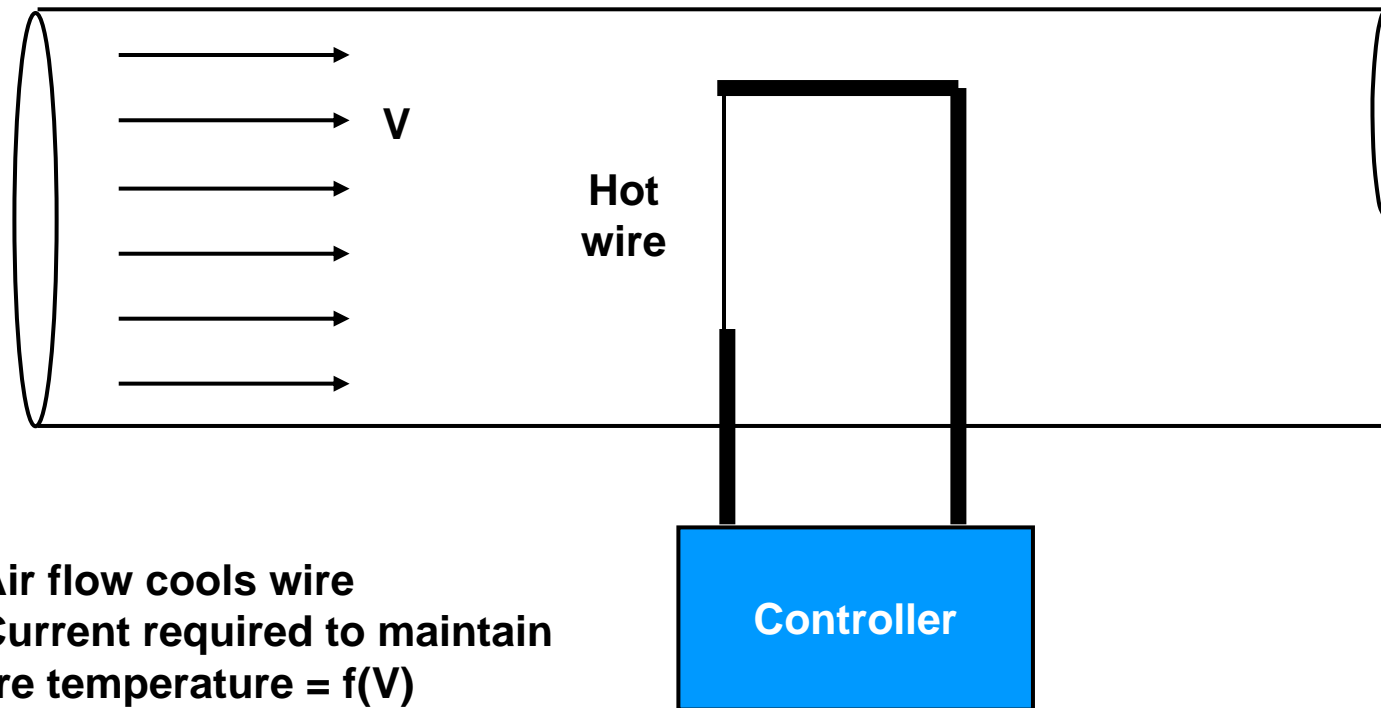


$$T_{1,2} = \frac{d}{\sin(\theta)(C + V \cos(\theta))}$$

$$T_{2,1} = \frac{d}{\sin(\theta)(C - V \cos(\theta))}$$

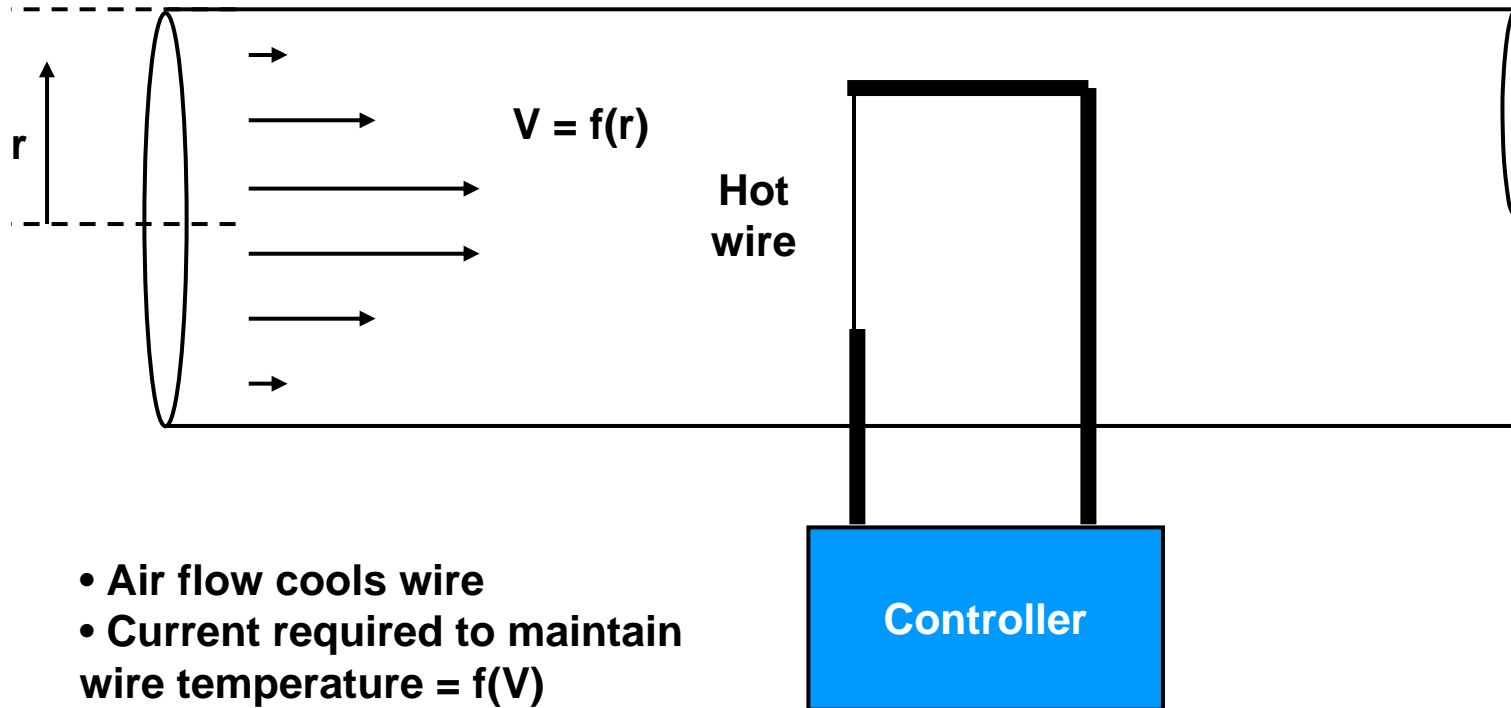
$$\frac{T_{1,2} - T_{2,1}}{T_{2,1}T_{2,1}} = \frac{2V \sin \theta \cos \theta}{d}$$

Hot-wire Air Mass Flowmeter



- Air flow cools wire
- Current required to maintain wire temperature = $f(V)$

Hot-wire Air Mass Flowmeter



Next time

- Finish measurement sensors